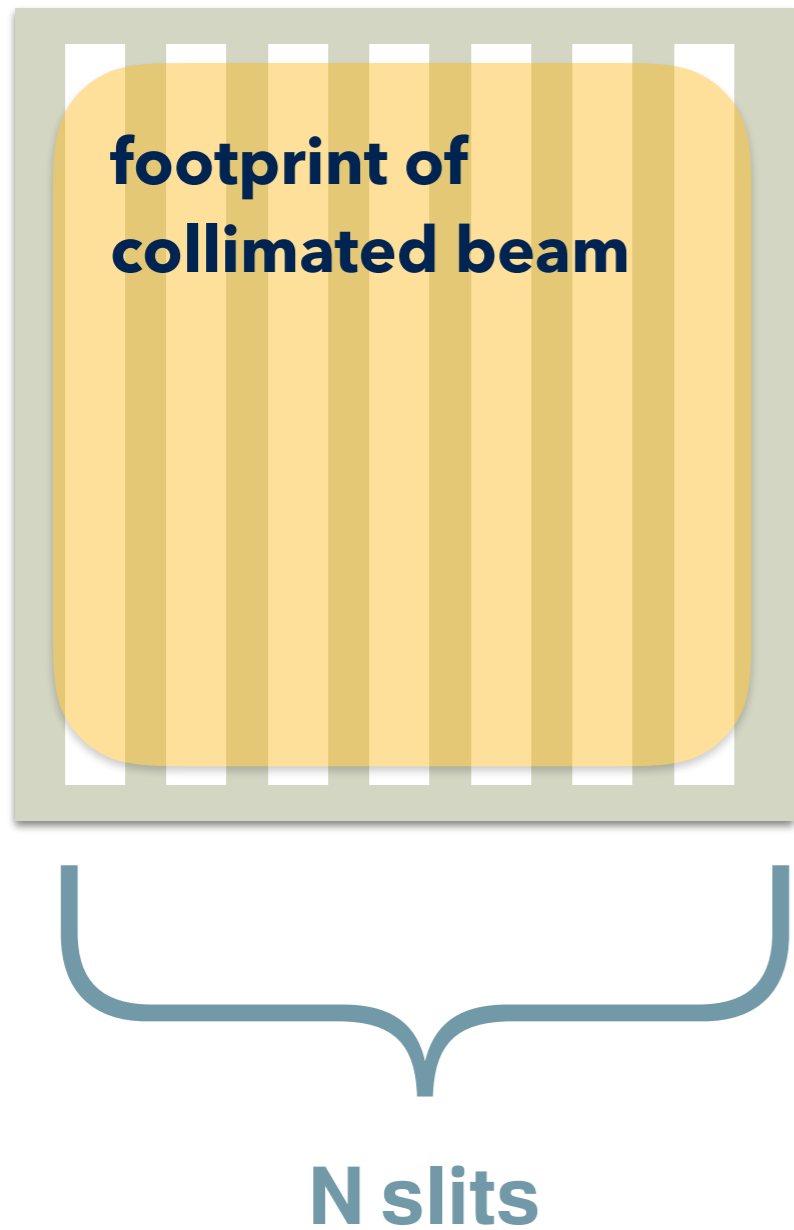


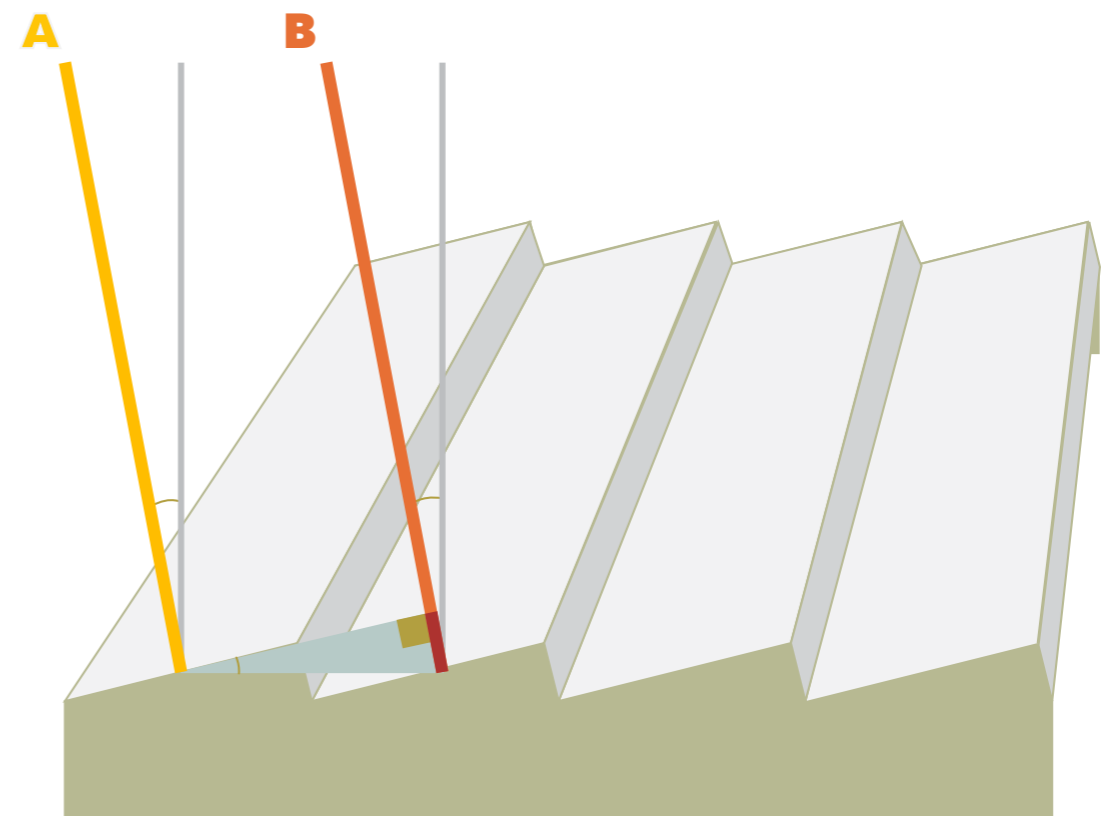
Diffraction grating



difference of pathlength

make certain color of light more intense toward certain direction

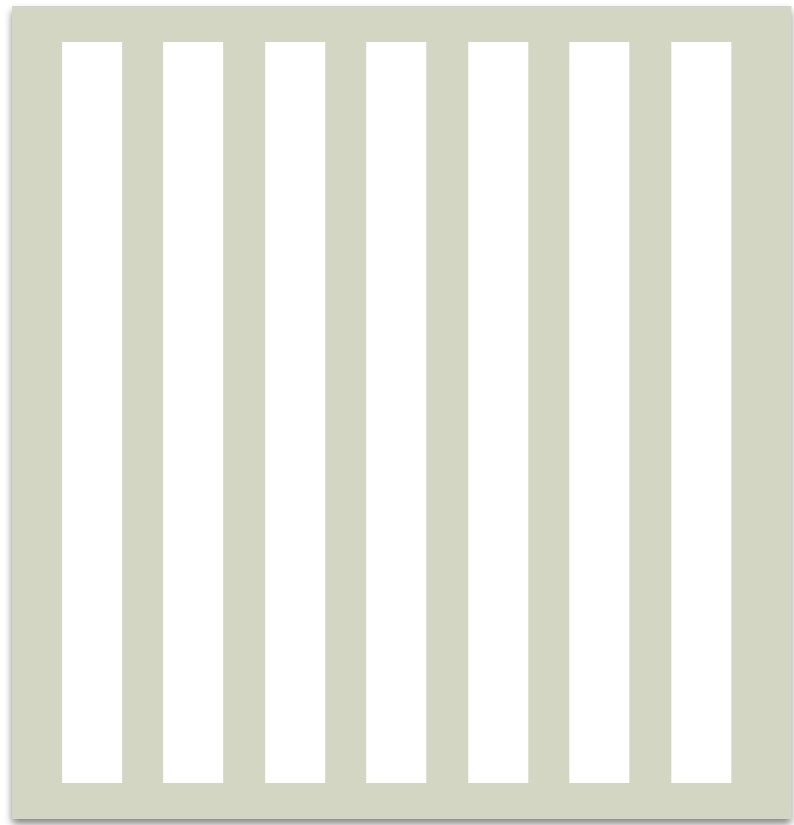
why not use just 2 slits?



because

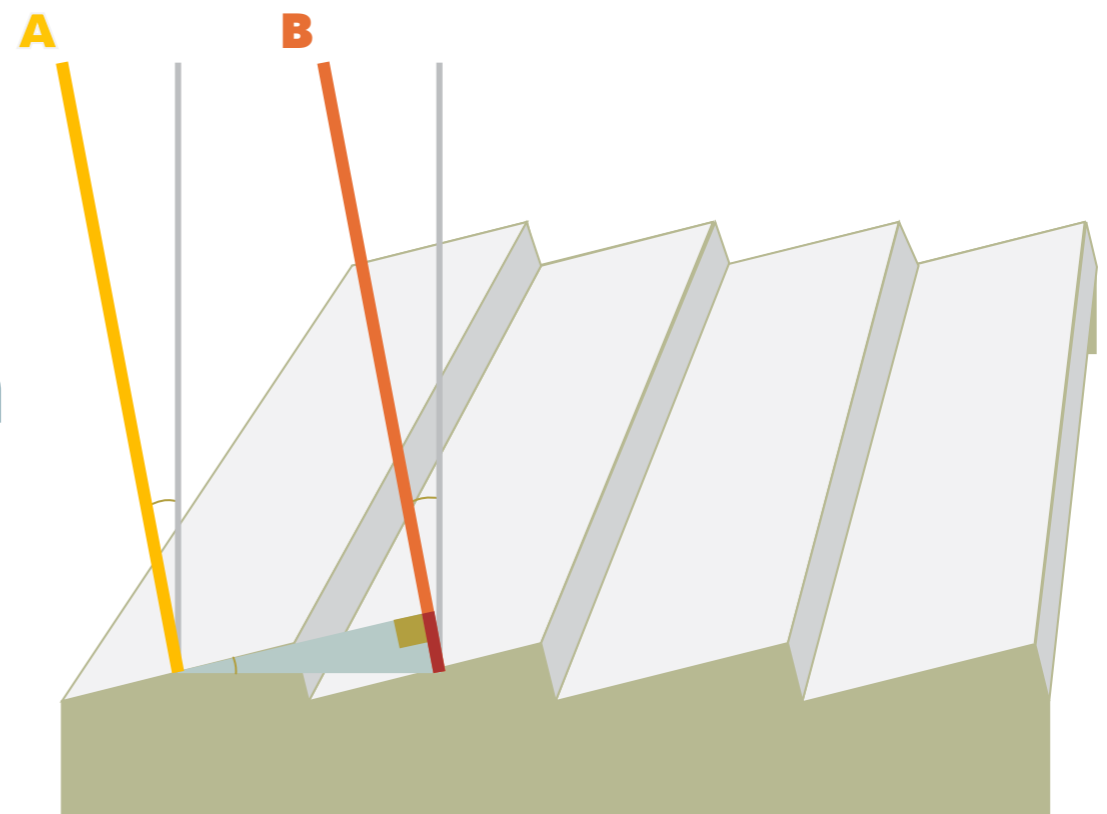
line Intensity goes up as $\propto N^2$

Diffraction grating



transmissive grating with slits
regular openings

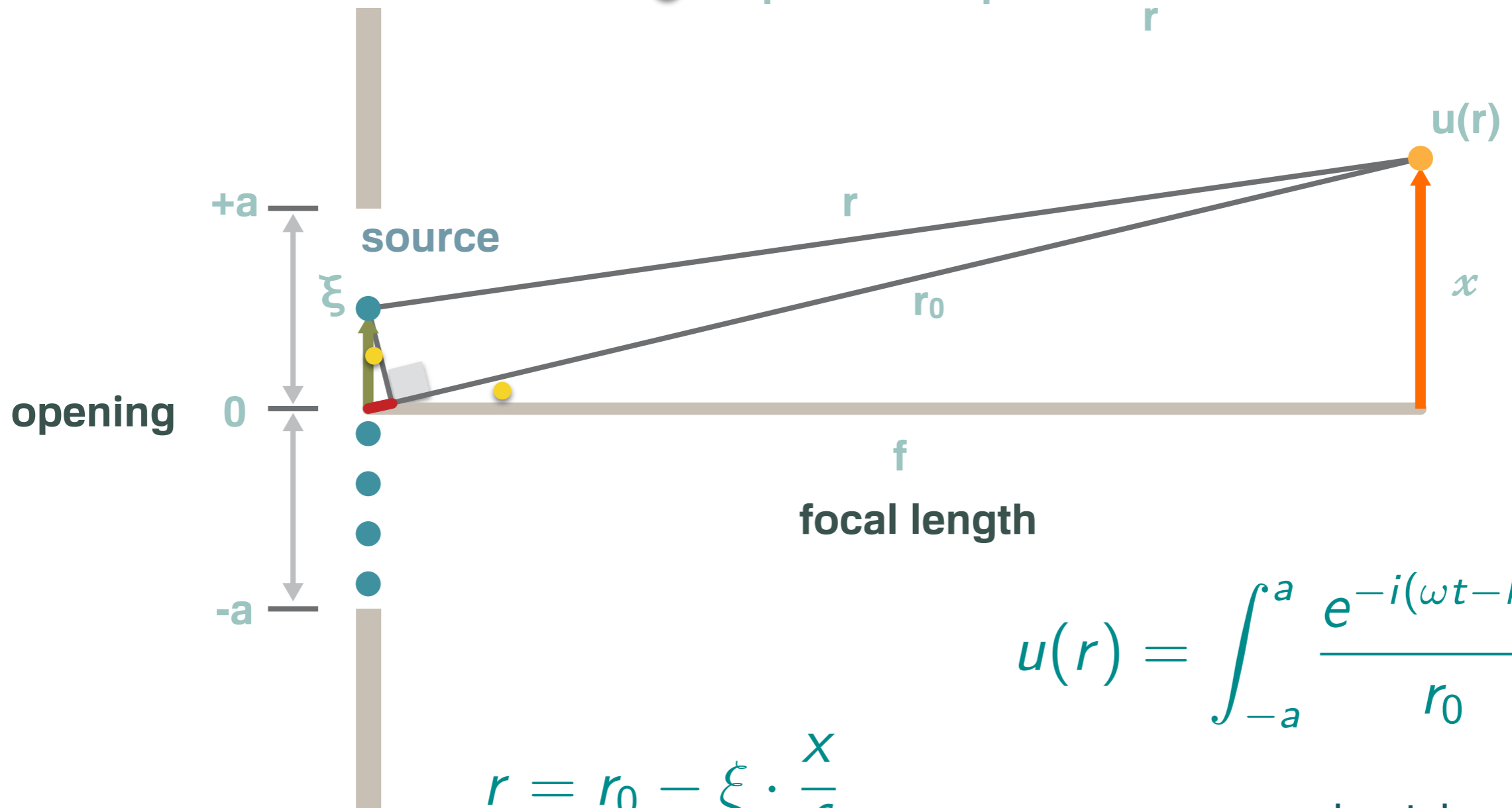
- 1 diffraction by a single slit
Fraunhofer diffraction
- 2 diffraction by a multiple slit
- 3 blazed grating



1 diffraction by a single slit

● $u_p(\xi) = e^{-i\omega t}$

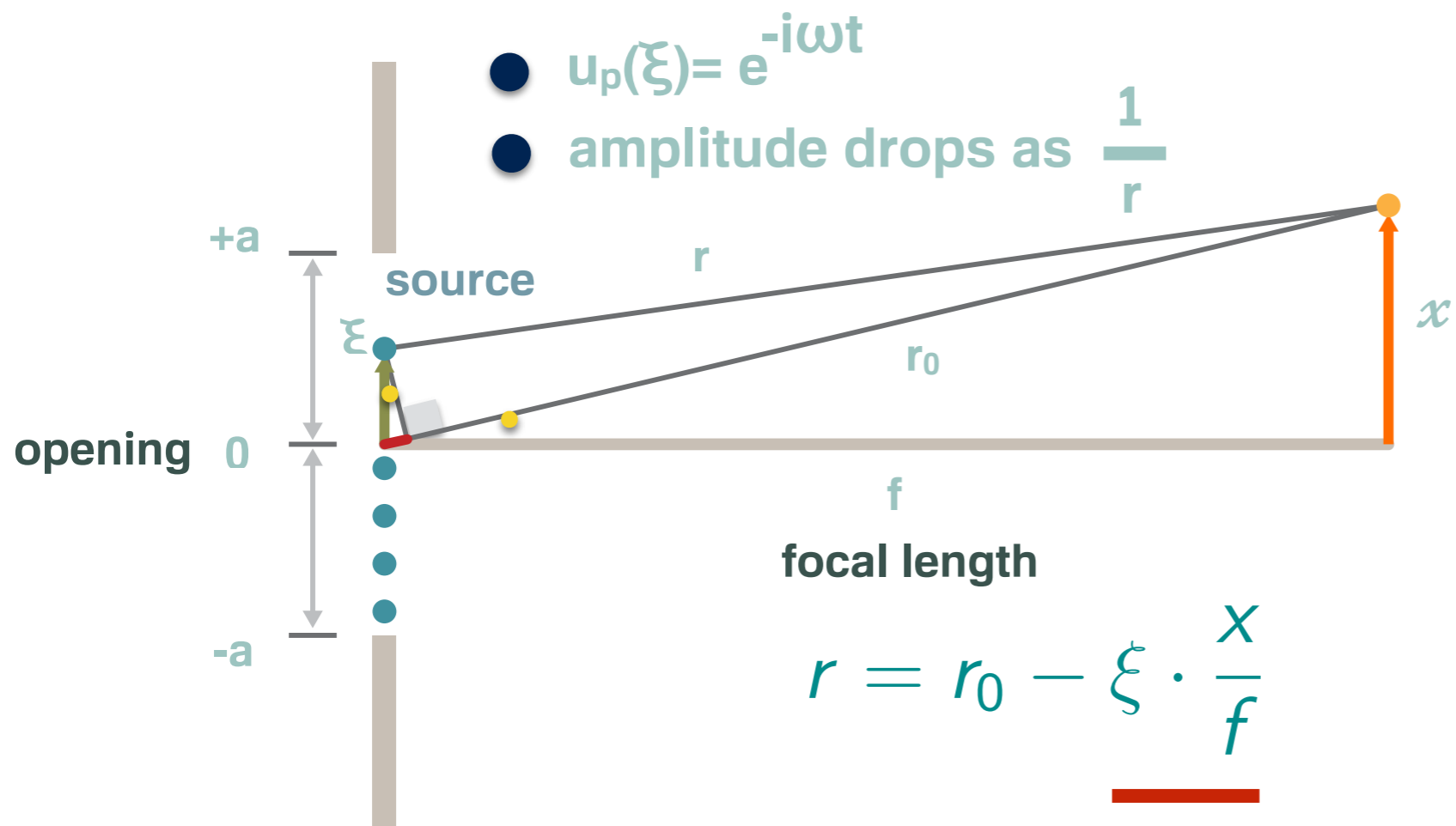
● amplitude drops as $\frac{1}{r}$



$$u(r) = \int_{-a}^a \frac{e^{-i(\omega t - kr)}}{r_0} d\xi$$

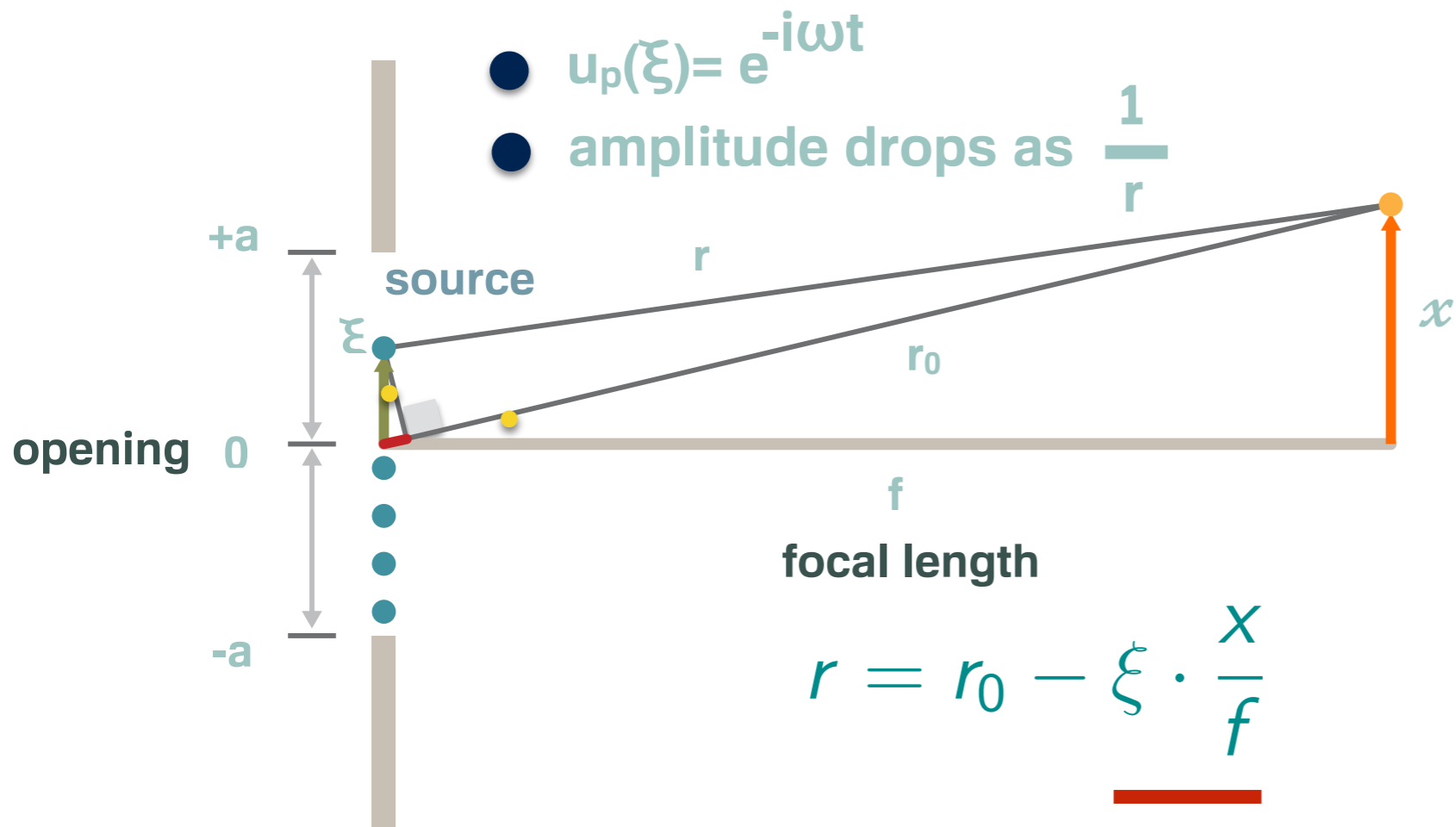
$$r = r_0 - \xi \cdot \frac{x}{f}$$

you have to be careful on phase part only



$$\begin{aligned}
 u(r) &= \int_{-a}^{+a} u_p(\xi) d\xi \\
 &= \frac{1}{r} \int_{-a}^{+a} e^{-i[\omega t - k(r_0 - \frac{\xi x}{f})]} d\xi \\
 &= \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} e^{-i\frac{k\xi x}{f}} d\xi \\
 &= \frac{e^{-i(\omega t - kr_0)}}{r} \frac{f}{-ikx} \left[e^{-\frac{ik\xi x}{f}} \right]_{-a}^{+a} \\
 &= \frac{e^{-i(\omega t - kr_0)}}{r} \frac{if}{kx} \left[e^{-\frac{ikax}{f}} - e^{\frac{ikax}{f}} \right]
 \end{aligned}$$

$$\frac{e^{i\theta} - e^{-i\theta}}{2} = \sin \theta$$



$$\begin{aligned}
 u(r) &= \int_{-a}^{+a} u_p(\xi) d\xi \\
 &= \frac{1}{r} \int_{-a}^{+a} e^{-i[\omega t - k(r_0 - \frac{\xi x}{f})]} d\xi \\
 &= \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} e^{-i\frac{k\xi x}{f}} d\xi \\
 &= \frac{e^{-i(\omega t - kr_0)}}{r} \frac{f}{-ikx} \left[e^{-\frac{ik\xi x}{f}} \right]_{-a}^{+a} \\
 &= \frac{e^{-i(\omega t - kr_0)}}{r} \frac{if}{kx} \left[e^{-\frac{ikax}{f}} - e^{\frac{ikax}{f}} \right]
 \end{aligned}$$

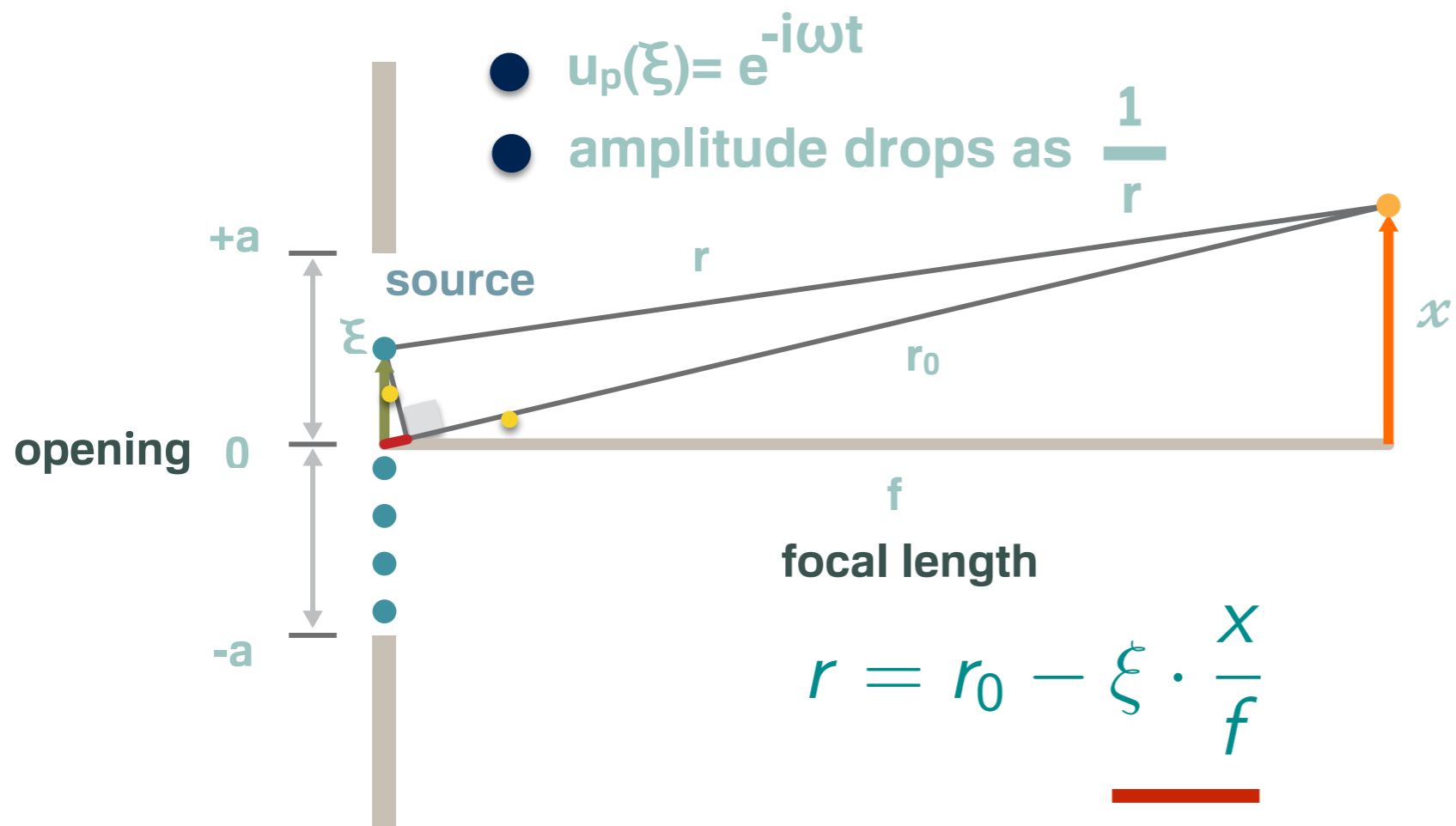
$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} \frac{-i2f}{kx} \sin\left(\frac{kax}{f}\right)$$

we want to make it

$$\frac{e^{i\theta} - e^{-i\theta}}{2} = \sin \theta$$

$$= \frac{e^{-i(\omega t - kr_0)}}{r} \frac{-i2f}{kx} \frac{kax}{f} \frac{\sin\left(\frac{kax}{f}\right)}{\frac{kax}{f}}$$

$$= \frac{e^{-i(\omega t - kr_0)}}{r} (-i2a) \frac{\sin\left(\frac{kax}{f}\right)}{\frac{kax}{f}}$$



$$\begin{aligned}
 u(r) &= \int_{-a}^{+a} u_p(\xi) d\xi \\
 &= \frac{1}{r} \int_{-a}^{+a} e^{-i[\omega t - k(r_0 - \frac{\xi x}{f})]} d\xi \\
 &= \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} e^{-i\frac{k\xi x}{f}} d\xi \\
 &= \frac{e^{-i(\omega t - kr_0)}}{r} \frac{f}{-ikx} \left[e^{-\frac{ik\xi x}{f}} \right]_{-a}^{+a} \\
 &= \frac{e^{-i(\omega t - kr_0)}}{r} \frac{if}{kx} \left[e^{-\frac{ikax}{f}} - e^{\frac{ikax}{f}} \right]
 \end{aligned}$$

$$I = |u(r)|^2 = \frac{4a^2}{r^2} \left(\frac{\sin \frac{kax}{f}}{\frac{kax}{f}} \right)^2$$

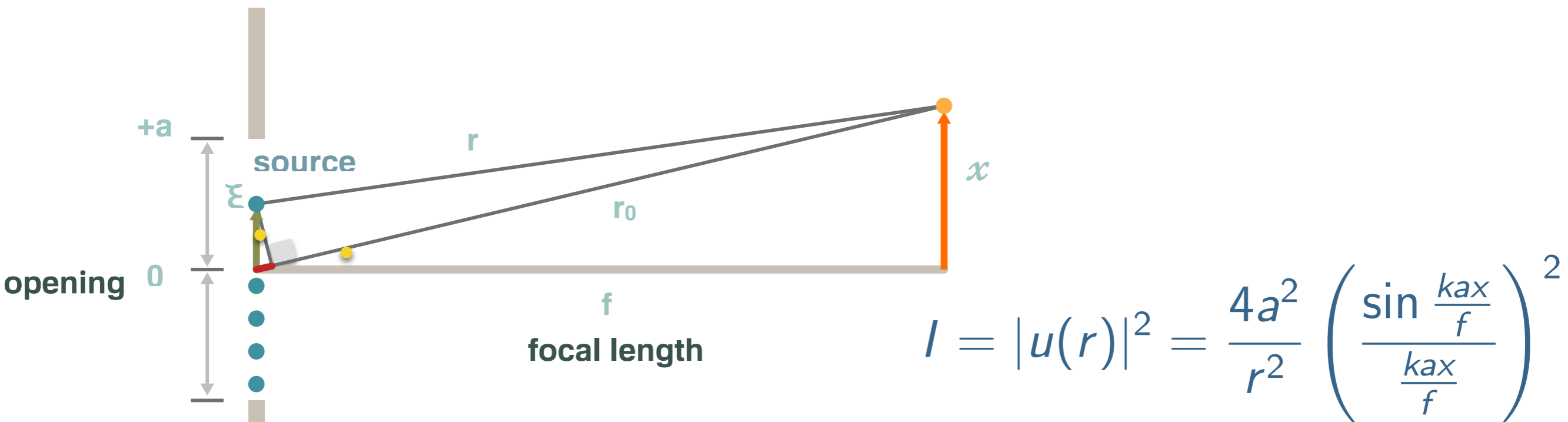
$$= \frac{4a^2}{r^2} \quad (x = 0)$$

on axis intensity

we want to make it

$$\frac{e^{i\theta} - e^{-i\theta}}{2} = \sin \theta$$

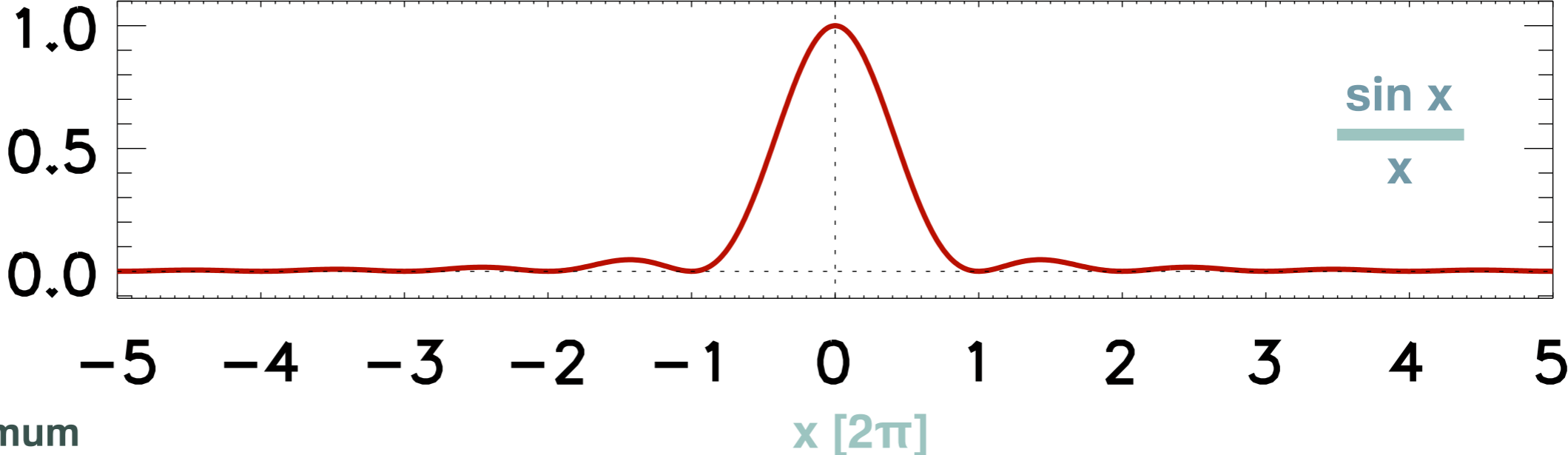
$$u(r) = \frac{\sin x}{x} \frac{e^{-i(\omega t - kr_0)}}{r} (-i2a) \frac{\sin \left(\frac{kax}{f} \right)}{\frac{kax}{f}}$$



$I=0$ when

$$\frac{kax}{f} = \pi$$

first minimum



$$\frac{2\pi ax}{f\lambda} = \pi$$

$$k = \frac{2\pi}{\lambda}$$

$$\frac{x}{f} = \frac{\lambda}{R}$$

angular resolution

wavelength / telescope aperture

Fraunhofer diffraction

- far field
- opening $\gg \lambda$

Fresnel diffraction
Sommerfeld solution

2 diffraction by a multiple slit

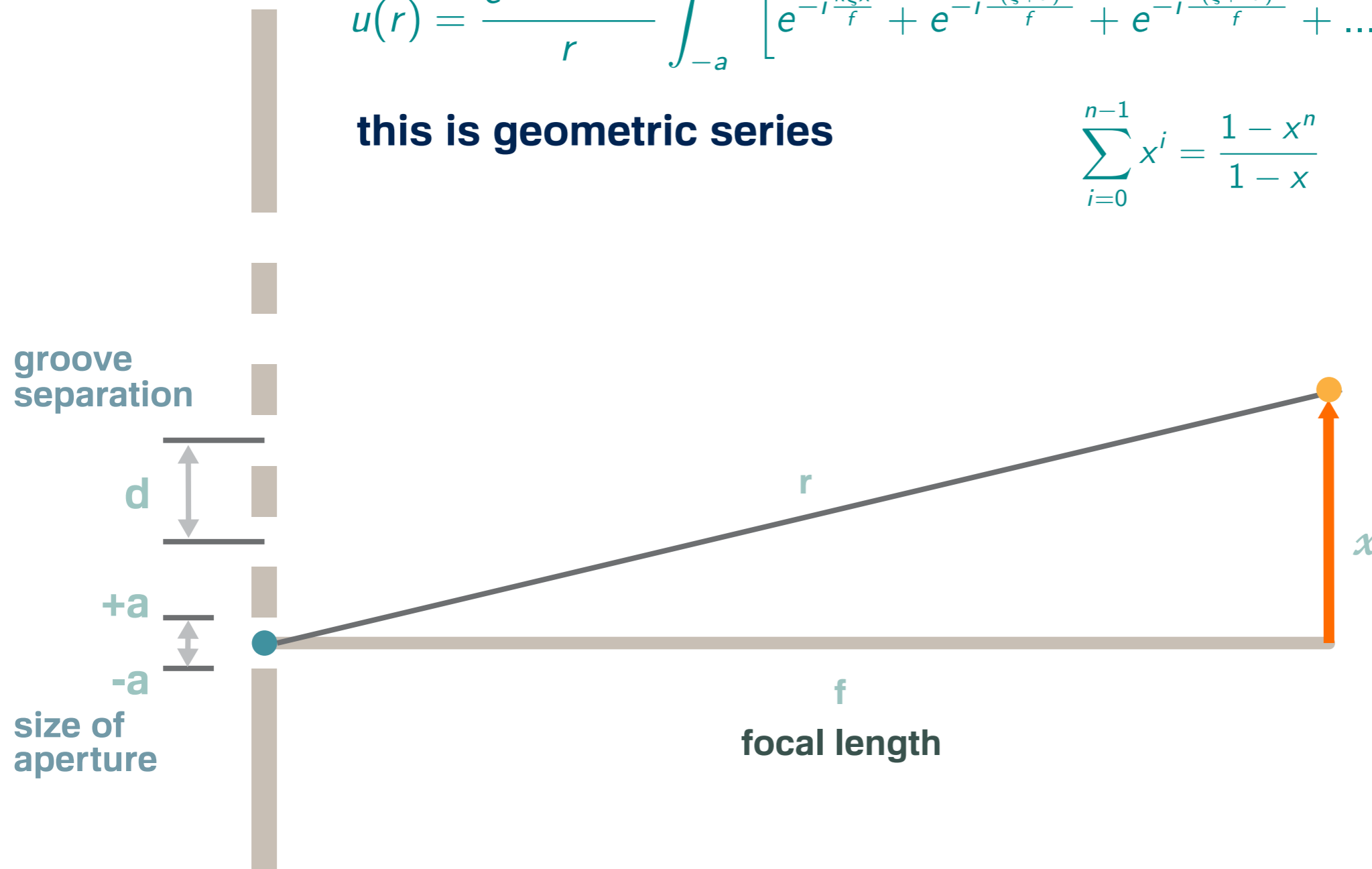
$$u(r) = \frac{1}{r} \int_{-a}^{+a} e^{-i[\omega t - k(r_0 - \frac{\xi x}{f})]} d\xi \quad \text{single slit}$$

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} \left[e^{-i\frac{k\xi x}{f}} + e^{-i\frac{k(\xi+d)x}{f}} + e^{-i\frac{k(\xi+2d)x}{f}} + \dots + e^{-i\frac{k(\xi+(N-1)d)x}{f}} \right] d\xi$$

this is geometric series

$$\sum_{i=0}^{n-1} x^i = \frac{1 - x^n}{1 - x}$$

N slits
 $x = e^{-\frac{ikxd}{f}}$



2 diffraction by a multiple slit

$$u(r) = \frac{1}{r} \int_{-a}^{+a} e^{-i[\omega t - k(r_0 - \frac{\xi x}{f})]} d\xi \quad \text{single slit}$$

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} \left[e^{-i\frac{k\xi x}{f}} + e^{-i\frac{k(\xi+d)x}{f}} + e^{-i\frac{k(\xi+2d)x}{f}} + \dots + e^{-i\frac{k(\xi+(N-1)d)x}{f}} \right] d\xi$$

this is geometric series

this part is same with single slit

$$\sum_{i=0}^{n-1} x^i = \frac{1 - x^n}{1 - x}$$

N slits

$$x = e^{-i\frac{kx d}{f}}$$

groove separation

d

+a

-a

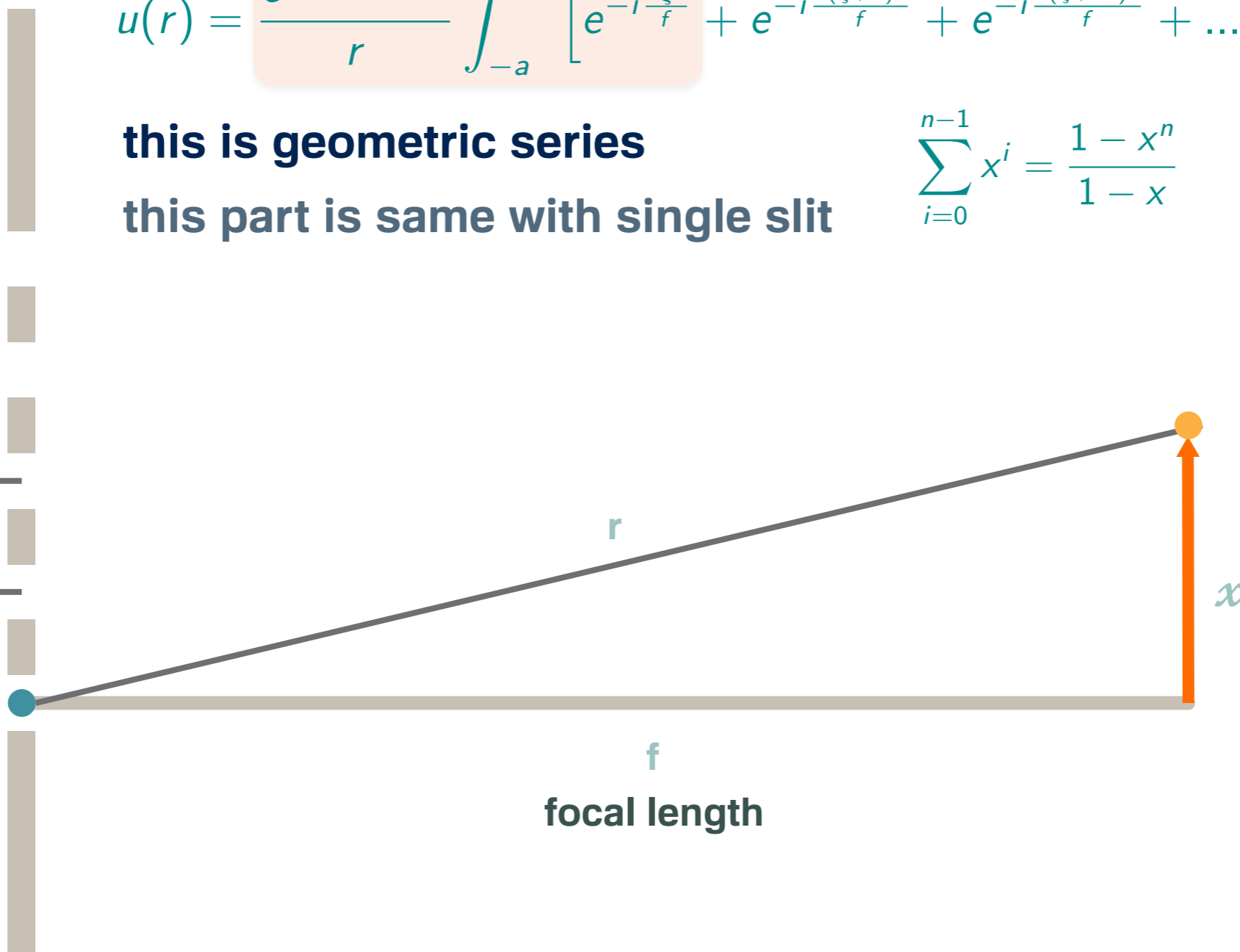
size of aperture

r

f

focal length

x



2 diffraction by a multiple slit

$$u(r) = \frac{1}{r} \int_{-a}^{+a} e^{-i[\omega t - k(r_0 - \frac{\xi x}{f})]} d\xi \quad \text{single slit}$$

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} \left[e^{-i\frac{k\xi x}{f}} + e^{-i\frac{k(\xi+d)x}{f}} + e^{-i\frac{k(\xi+2d)x}{f}} + \dots + e^{-i\frac{k(\xi+(N-1)d)x}{f}} \right] d\xi$$

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$$\sum_{i=0}^{n-1} x^i = \frac{1 - x^n}{1 - x}$$

N slits

$$x = e^{-\frac{ikxd}{f}}$$

groove separation

d

+a

-a

size of aperture

r

f

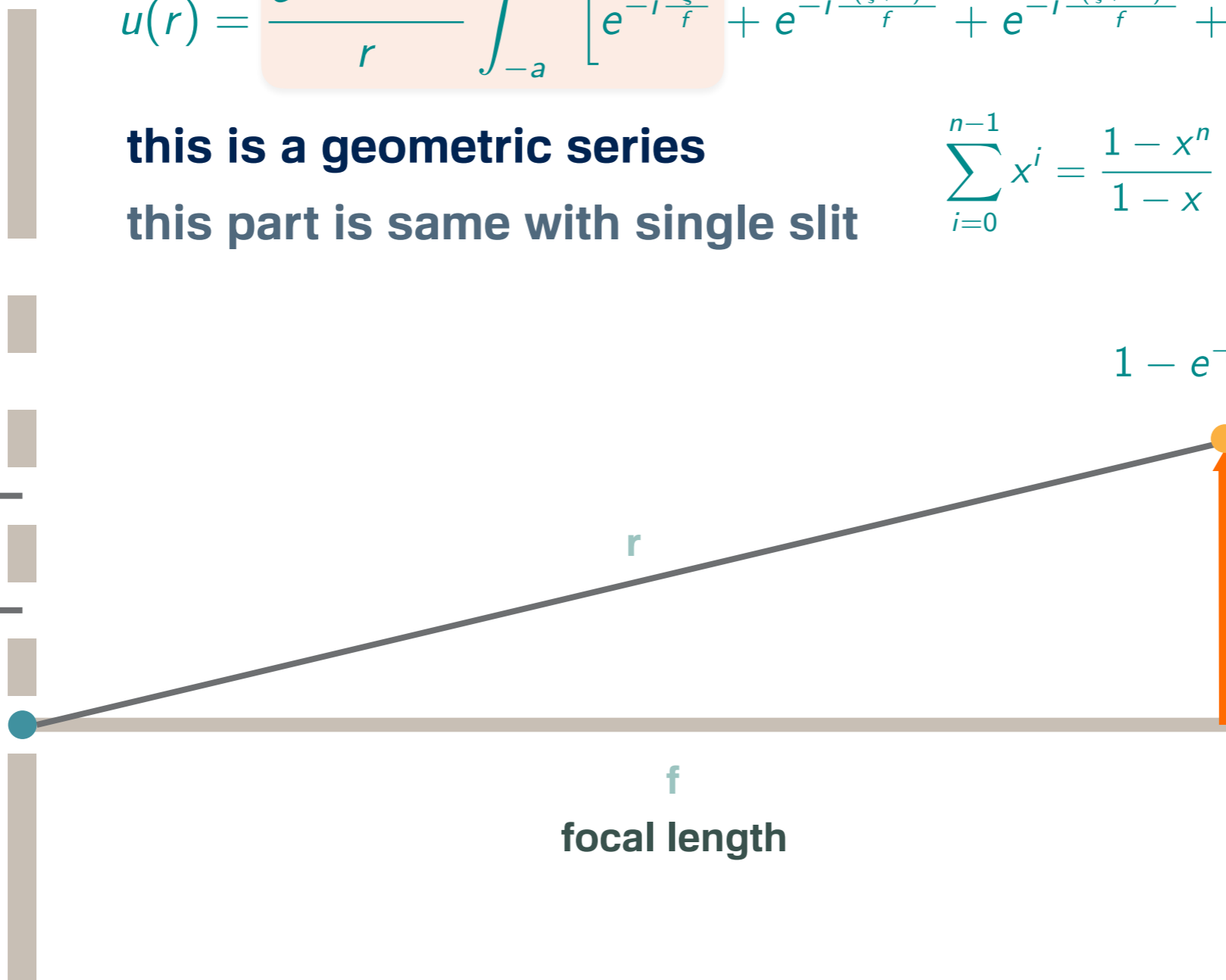
focal length

$$1 - e^{-i\theta} = e^{-\frac{i\theta}{2}} \left(e^{\frac{i\theta}{2}} - e^{-\frac{i\theta}{2}} \right)$$

$$= e^{-\frac{i\theta}{2}} \cdot 2 \sin \left(\frac{\theta}{2} \right)$$

x

$$\theta = \frac{kxd}{f}$$



2 diffraction by a multiple slit

$$u(r) = \frac{1}{r} \int_{-a}^{+a} e^{-i[\omega t - k(r_0 - \frac{\xi x}{f})]} d\xi \quad \text{one slit}$$

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} \left[e^{-i\frac{k\xi x}{f}} + e^{-i\frac{k(\xi+d)x}{f}} + e^{-i\frac{k(\xi+2d)x}{f}} + \dots + e^{-i\frac{k(\xi+(N-1)d)x}{f}} \right] d\xi$$

this is a geometric series

this part is same with single slit

$$\sum_{i=0}^{n-1} x^i = \frac{1 - x^n}{1 - x}$$

N slits

$$x = e^{-\frac{ikxd}{f}}$$

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} \frac{1 - e^{-\frac{ikNxd}{f}}}{1 - e^{-\frac{ikxc}{f}}} \cdot e^{-\frac{ik\xi x}{f}} d\xi$$

groove separation

d

+a

-a

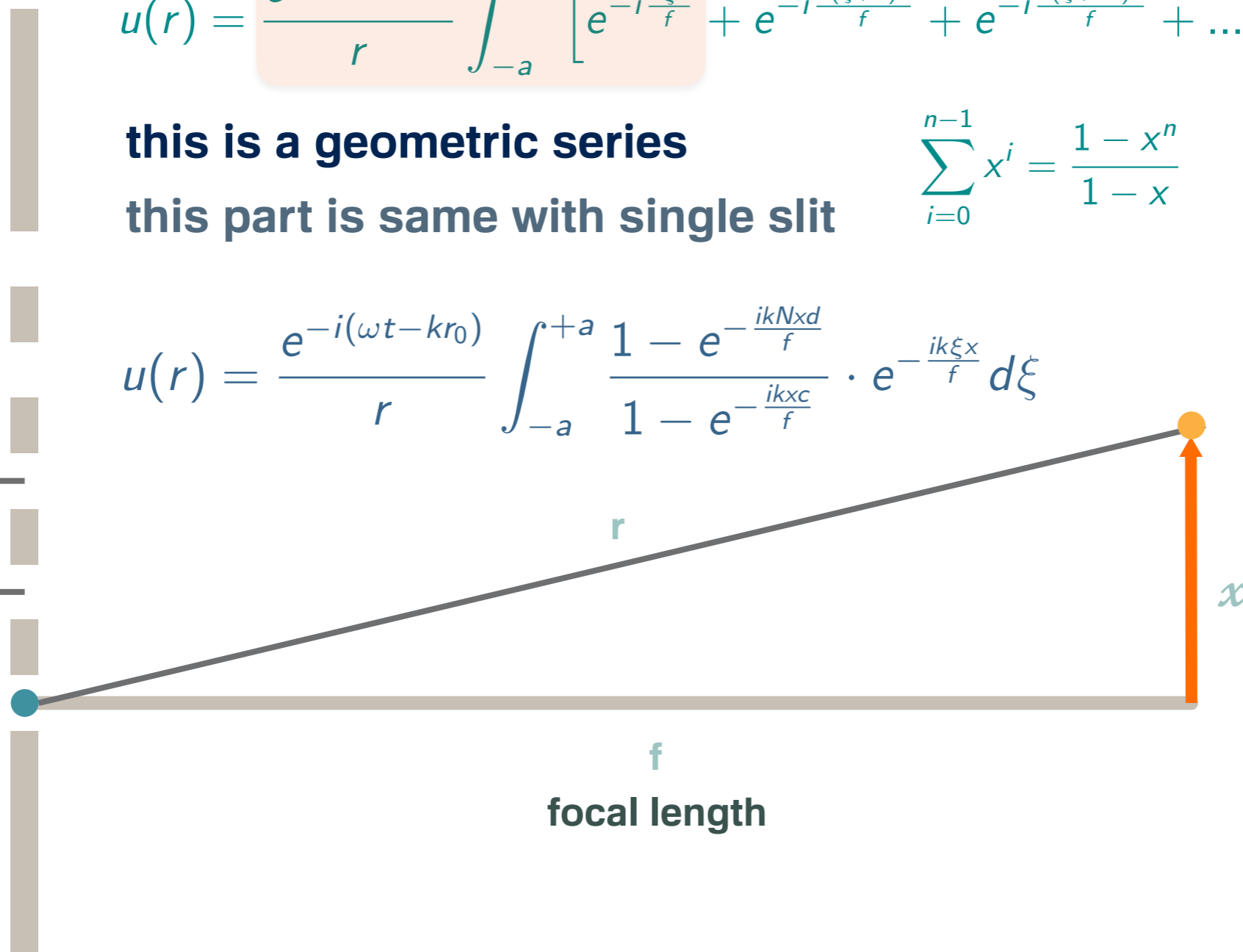
size of aperture

r

x

f

focal length



2 diffraction by a multiple slit

$$u(r) = \frac{1}{r} \int_{-a}^{+a} e^{-i[\omega t - k(r_0 - \frac{\xi x}{f})]} d\xi \quad \text{one slit}$$

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} \left[e^{-i\frac{k\xi x}{f}} + e^{-i\frac{k(\xi+d)x}{f}} + e^{-i\frac{k(\xi+2d)x}{f}} + \dots + e^{-i\frac{k(\xi+(N-1)d)x}{f}} \right] d\xi$$

this is a geometric series

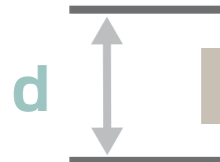
this part is same with single slit

$$\sum_{i=0}^{n-1} x^i = \frac{1-x^n}{1-x}$$

N slits

$$x = e^{-\frac{ikxd}{f}}$$

groove separation



+a
-a

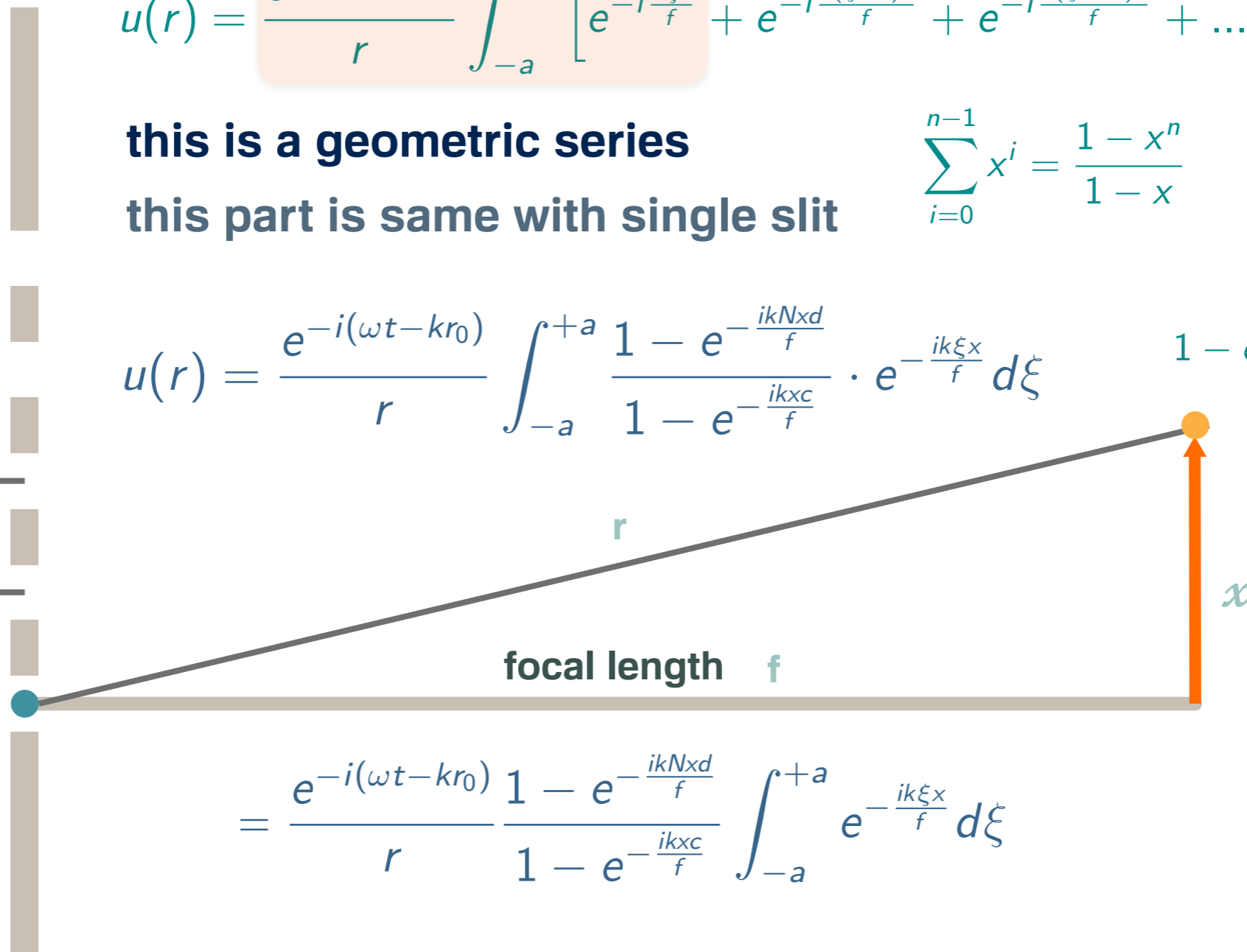
size of aperture

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} \frac{1 - e^{-\frac{ikNxd}{f}}}{1 - e^{-\frac{ikxc}{f}}} \cdot e^{-\frac{ik\xi x}{f}} d\xi$$

$$1 - e^{-i\theta} = e^{-\frac{i\theta}{2}} \left(e^{\frac{i\theta}{2}} - e^{-\frac{i\theta}{2}} \right)$$

$$= e^{-\frac{i\theta}{2}} \cdot 2 \sin \left(\frac{\theta}{2} \right)$$

$$\theta = \frac{kxd}{f}$$



$$= \frac{e^{-i(\omega t - kr_0)}}{r} \frac{1 - e^{-\frac{ikNxd}{f}}}{1 - e^{-\frac{ikxc}{f}}} \int_{-a}^{+a} e^{-\frac{ik\xi x}{f}} d\xi$$

2 diffraction by a multiple slit

$$u(r) = \frac{1}{r} \int_{-a}^{+a} e^{-i[\omega t - k(r_0 - \frac{\xi x}{f})]} d\xi \quad \text{one slit}$$

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} \left[e^{-i\frac{k\xi x}{f}} + e^{-i\frac{k(\xi+d)x}{f}} + e^{-i\frac{k(\xi+2d)x}{f}} + \dots + e^{-i\frac{k(\xi+(N-1)d)x}{f}} \right] d\xi$$

this is a geometric series

this part is same with single slit

$$\sum_{i=0}^{n-1} x^i = \frac{1-x^n}{1-x}$$

N slits
 $x = e^{-i\frac{kxd}{f}}$

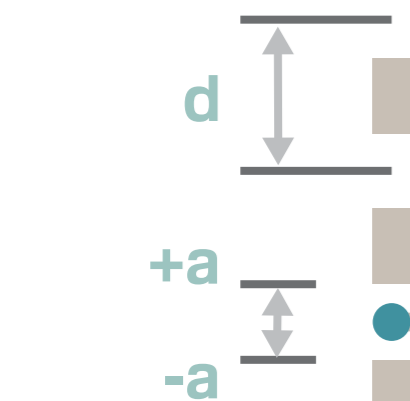
groove separation

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} \frac{1 - e^{-i\frac{kNxd}{f}}}{1 - e^{-i\frac{kxc}{f}}} \cdot e^{-i\frac{k\xi x}{f}} d\xi$$

$$1 - e^{-i\theta} = e^{-\frac{i\theta}{2}} \left(e^{\frac{i\theta}{2}} - e^{-\frac{i\theta}{2}} \right)$$

$$= e^{-\frac{i\theta}{2}} \cdot 2 \sin \left(\frac{\theta}{2} \right)$$

$$\theta = \frac{kxd}{f}$$



size of aperture

$$= \frac{e^{-i(\omega t - kr_0)}}{r} \frac{1 - e^{-i\frac{kNxd}{f}}}{1 - e^{-i\frac{kxc}{f}}} \int_{-a}^{+a} e^{-i\frac{k\xi x}{f}} d\xi$$

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} (-i2a) \frac{\sin \left(\frac{kax}{f} \right)}{\frac{kax}{f}}$$

2 diffraction by a multiple slit

$$u(r) = \frac{1}{r} \int_{-a}^{+a} e^{-i[\omega t - k(r_0 - \frac{\xi x}{f})]} d\xi \quad \text{one slit}$$

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} \left[e^{-i\frac{k\xi x}{f}} + e^{-i\frac{k(\xi+d)x}{f}} + e^{-i\frac{k(\xi+2d)x}{f}} + \dots + e^{-i\frac{k(\xi+(N-1)d)x}{f}} \right] d\xi$$

this is a geometric series

this part is same with single slit

$$\sum_{i=0}^{n-1} x^i = \frac{1-x^n}{1-x}$$

N slits
 $x = e^{-\frac{ikxd}{f}}$

groove separation

d

+a

-a

size of aperture

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} \int_{-a}^{+a} \frac{1 - e^{-\frac{ikNxd}{f}}}{1 - e^{-\frac{ikxc}{f}}} \cdot e^{-\frac{ik\xi x}{f}} d\xi$$

$$1 - e^{-i\theta} = e^{-\frac{i\theta}{2}} \left(e^{\frac{i\theta}{2}} - e^{-\frac{i\theta}{2}} \right)$$

$$= e^{-\frac{i\theta}{2}} \cdot 2 \sin \left(\frac{\theta}{2} \right)$$

$$\theta = \frac{kxd}{f}$$

focal length f

$$= \frac{e^{-i(\omega t - kr_0)}}{r} \frac{1 - e^{-\frac{ikNxd}{f}}}{1 - e^{-\frac{ikxc}{f}}} \int_{-a}^{+a} e^{-\frac{ik\xi x}{f}} d\xi$$

$$u(r) = \frac{e^{-i(\omega t - kr_0)}}{r} (-i2a) \frac{\sin \left(\frac{kax}{f} \right)}{\frac{kax}{f}} = \frac{e^{-i(\omega t - kr_0)}}{r} \frac{e^{-\frac{iN\theta}{2f}} \cdot 2 \sin \frac{N\theta}{2}}{e^{-\frac{i\theta}{2f}} \cdot 2 \sin \frac{\theta}{2}} \cdot (-i2a) \frac{\sin \left(\frac{kax}{f} \right)}{\frac{kax}{f}}$$

2 diffraction by a multiple slit

$$u(r) = \frac{e^{-i(\omega t - kr_0)} e^{-\frac{iN\theta}{2f}} \cdot 2 \sin \frac{N\theta}{2}}{r e^{-\frac{i\theta}{2f}} \cdot 2 \sin \frac{\theta}{2}} \cdot (-i2a) \frac{\sin \left(\frac{kax}{f} \right)}{\frac{kax}{f}}$$

$$I = |u(r)|^2 = \frac{4a^2}{r^2} \left(\frac{\sin \frac{N\theta}{2}}{\sin \frac{\theta}{2}} \right)^2 \left(\frac{\sin \frac{kax}{f}}{\frac{kax}{f}} \right)^2$$

groove
separation

d

+a

-a

size of
aperture

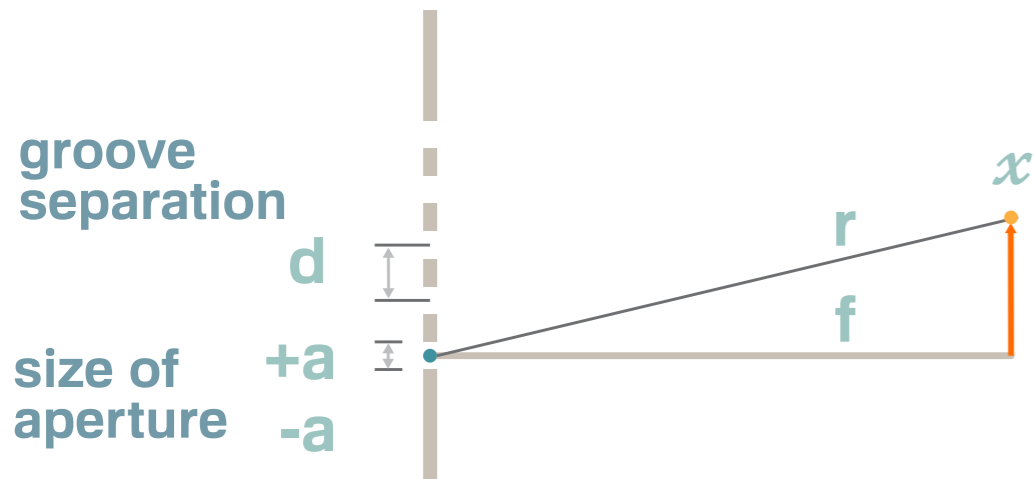
focal length f

$u(r)$

x

$$I = |u(r)|^2 = \frac{4a^2 N^2}{r^2} \left(\frac{\sin \frac{N\theta}{2}}{N \sin \frac{\theta}{2}} \right)^2 \left(\frac{\sin \frac{kax}{f}}{\frac{kax}{f}} \right)^2$$





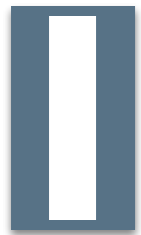
N slits

$$I = |u(r)|^2 = \frac{4a^2 N^2}{r^2} \left(\frac{\sin \frac{N\theta}{2}}{N \sin \frac{\theta}{2}} \right)^2 \left(\frac{\sin \frac{kax}{f}}{\frac{kax}{f}} \right)^2$$



$$\frac{\sin Nx}{\sin x} \rightarrow N \quad (x \rightarrow 0)$$

single slit



$$I = |u(r)|^2 = \frac{4a^2}{r^2} \left(\frac{\sin \frac{kax}{f}}{\frac{kax}{f}} \right)^2$$

$$= \frac{4a^2}{r^2} \quad (x = 0)$$

2 show this.

$$= \frac{4a^2 N^2}{r^2} \quad (x = 0)$$

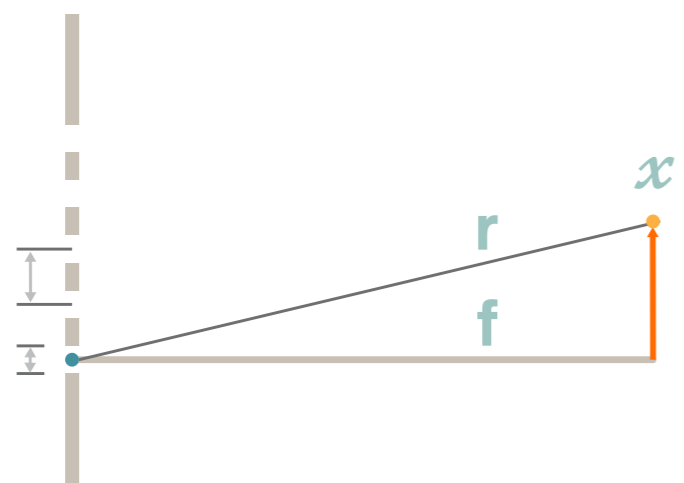
Intensity goes N^2 instead of N

groove separation

d

size of aperture

$+a$
 $-a$



fast frequency

$$I = |u(r)|^2 = \frac{4a^2}{r^2} \left(\frac{\sin \frac{N\theta}{2}}{\sin \frac{\theta}{2}} \right)^2 \left(\frac{\sin \frac{kax}{f}}{\frac{kax}{f}} \right)^2$$

slow frequency

$\sin Nx$

$/$
 $\sin x$

0

-2

-1

0

1

2

$N = 4$

0

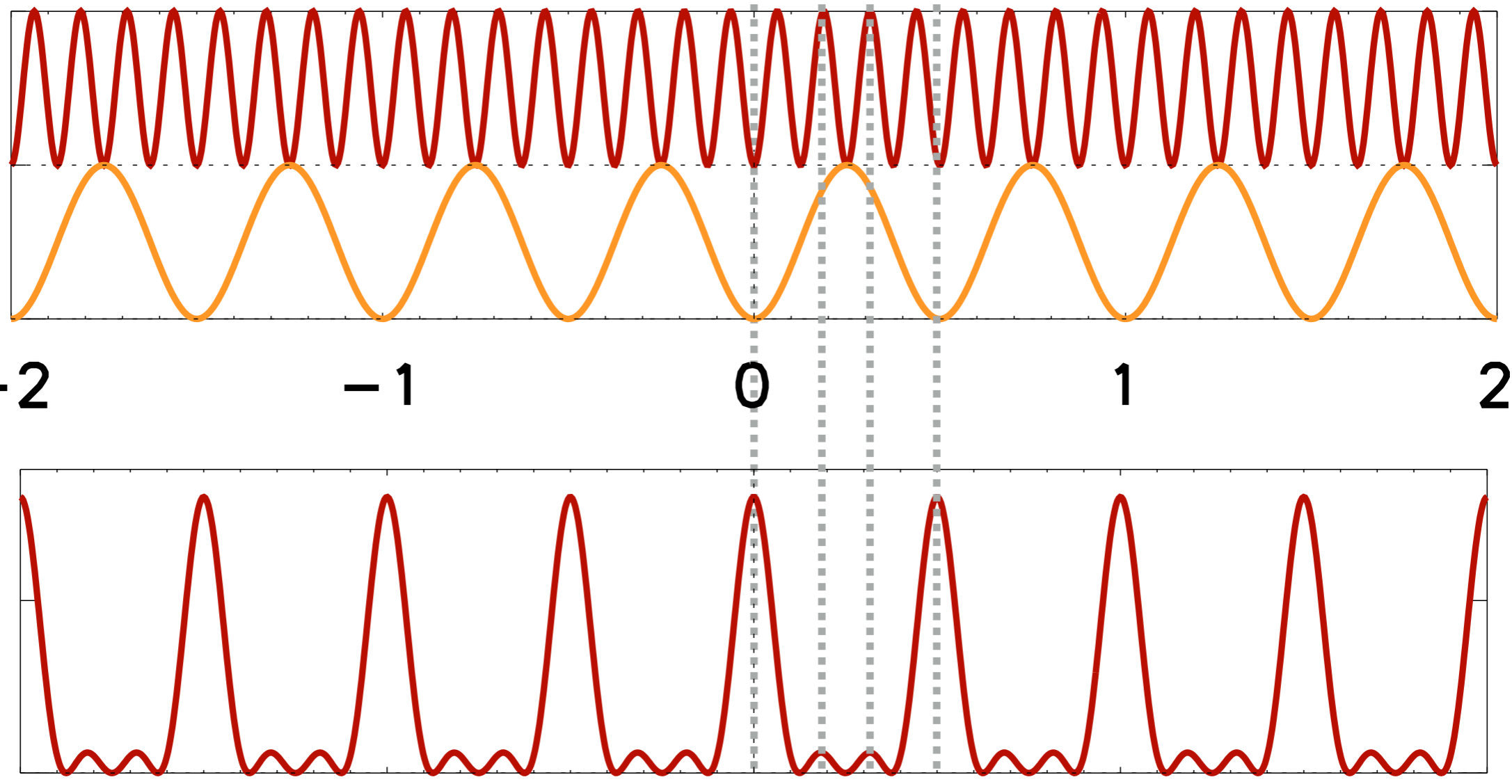
-2

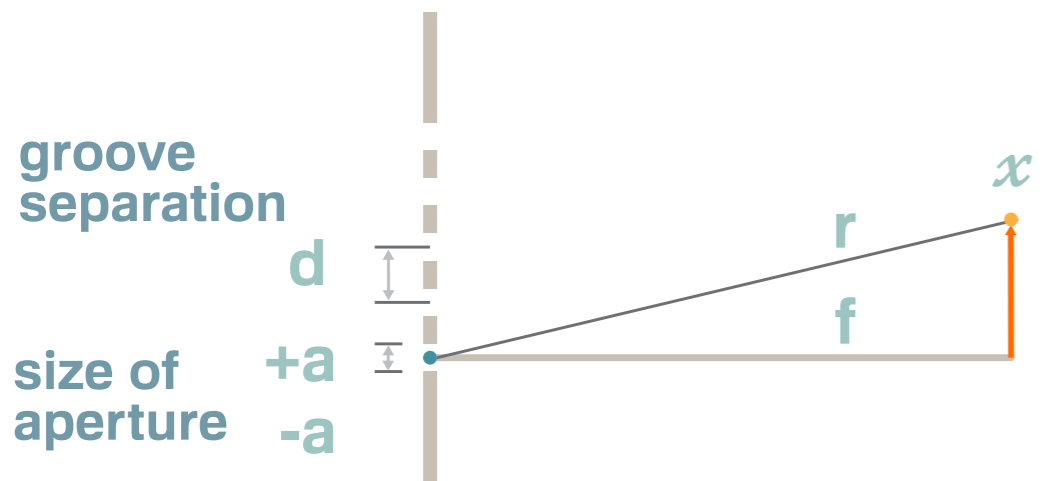
-1

0

1

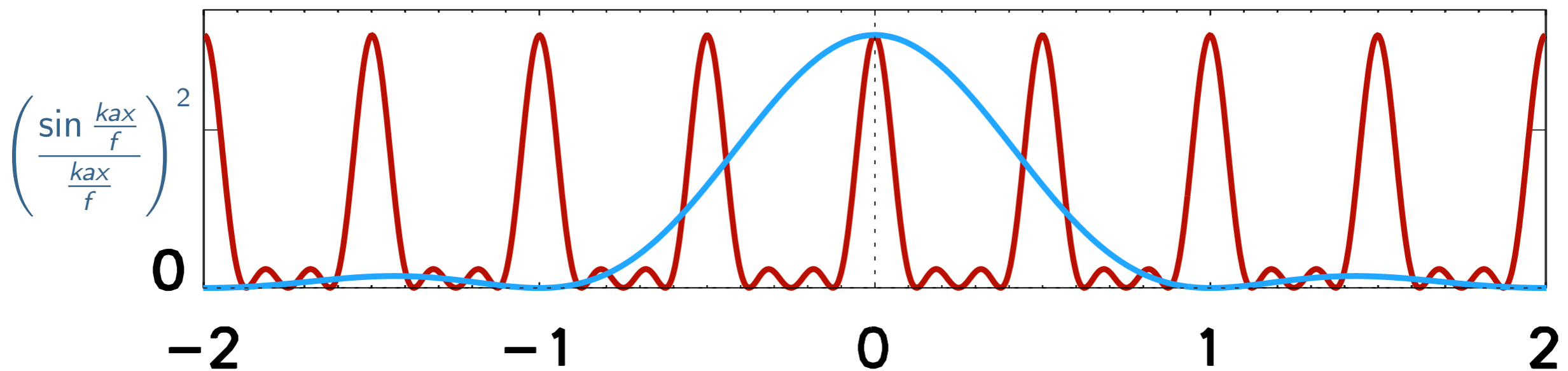
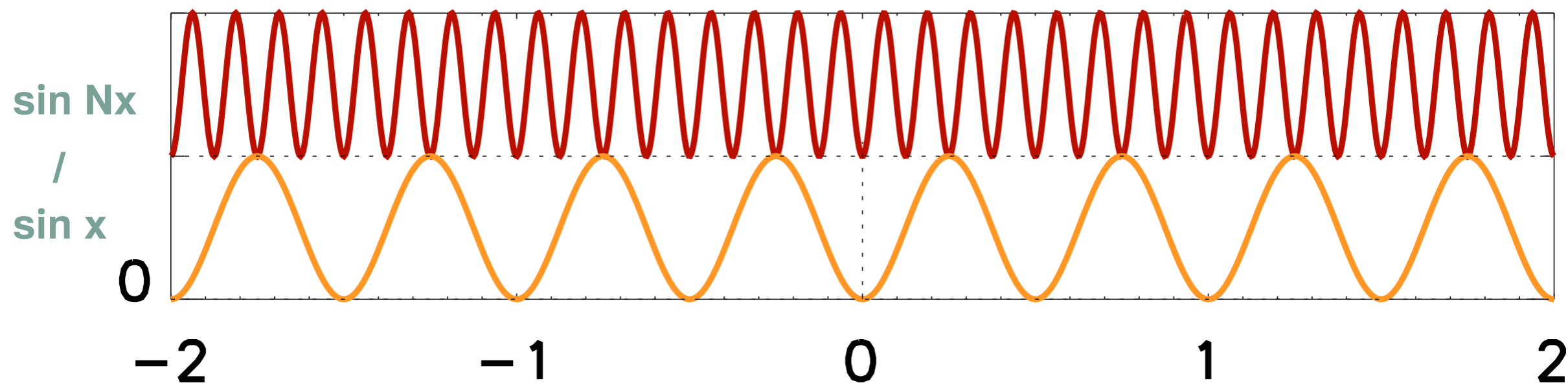
2

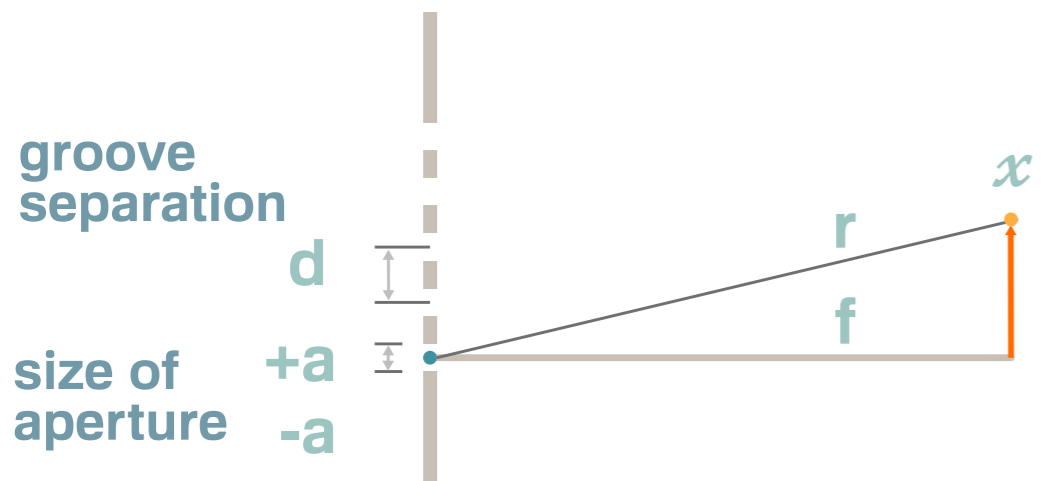




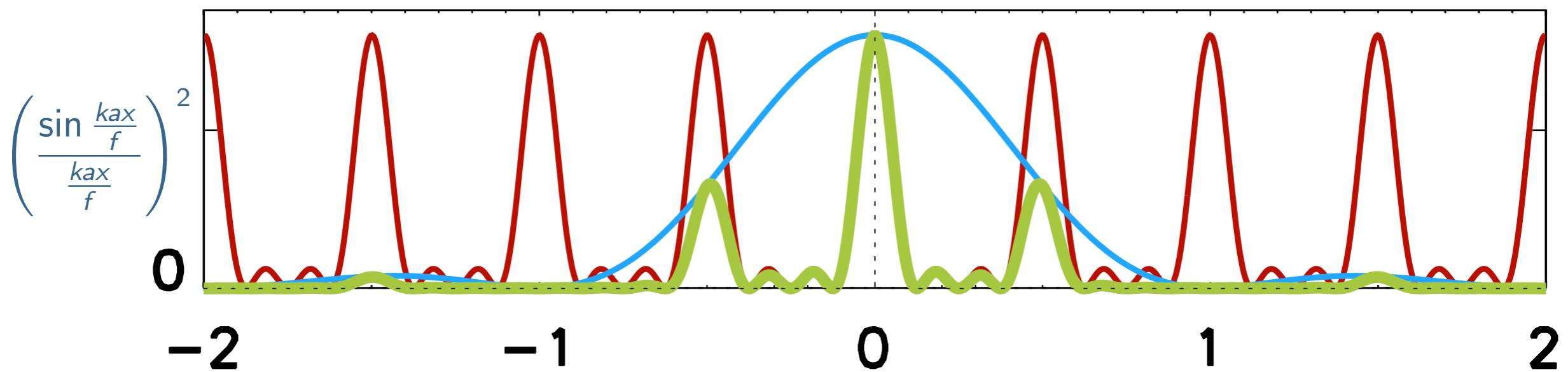
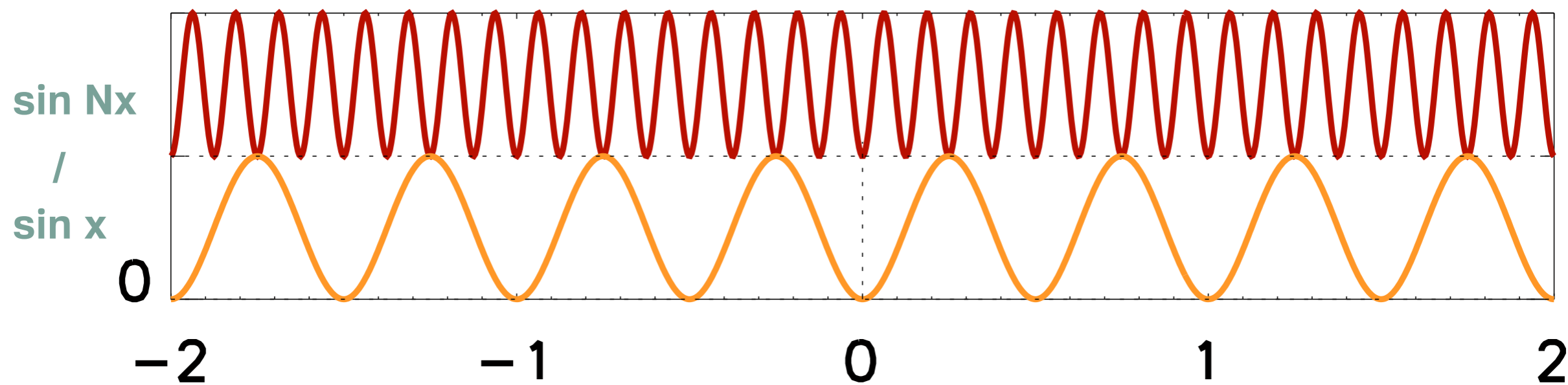
$$I = |u(r)|^2 = \frac{4a^2}{r^2} \left(\frac{\sin \frac{N\theta}{2}}{\sin \frac{\theta}{2}} \right)^2 \left(\frac{\sin \frac{kax}{f}}{\frac{kax}{f}} \right)^2$$

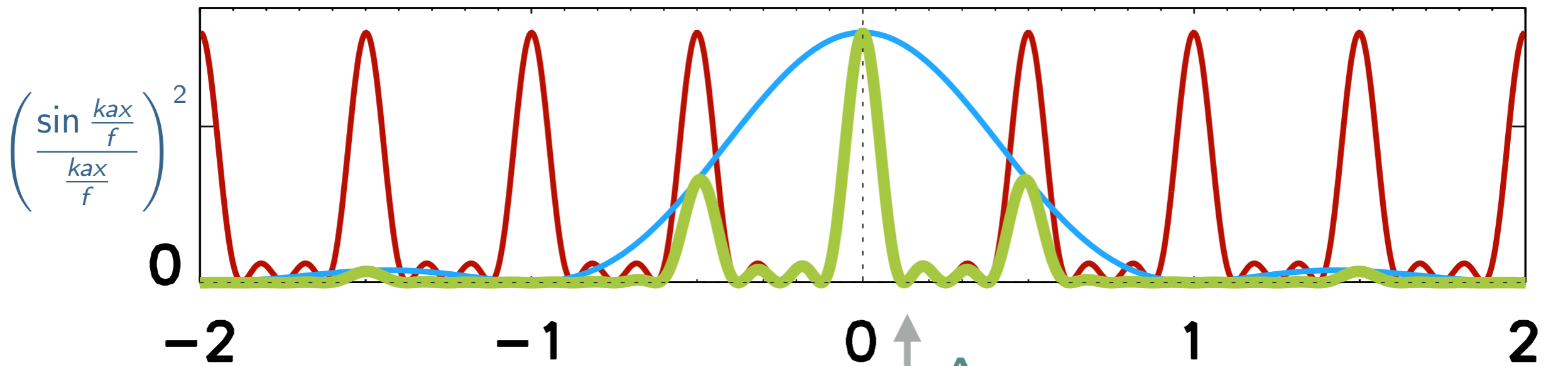
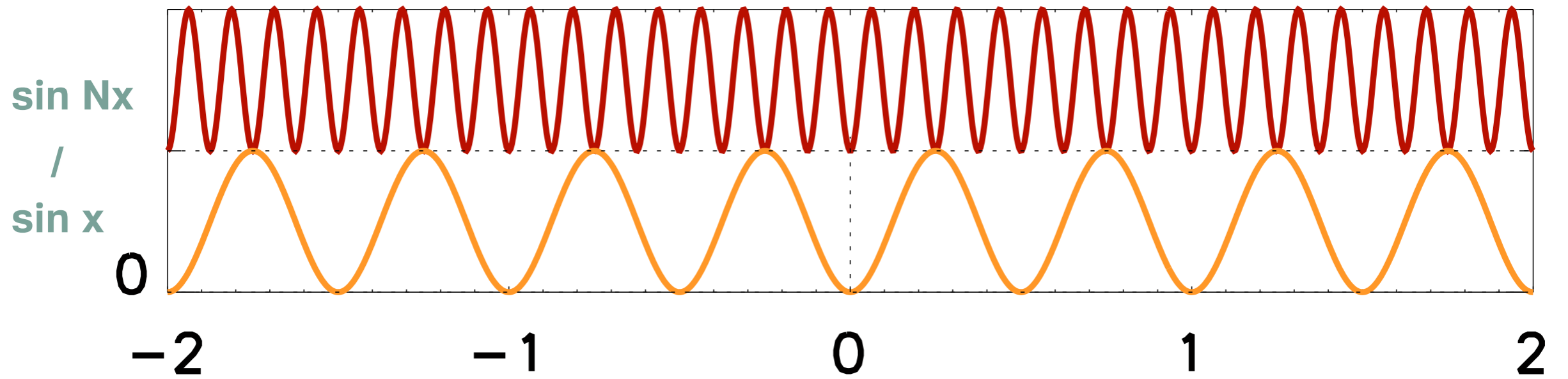
convolution





$$I = |u(r)|^2 = \frac{4a^2}{r^2} \left(\frac{\sin \frac{N\theta}{2}}{\sin \frac{\theta}{2}} \right)^2 \left(\frac{\sin \frac{kax}{f}}{\frac{kax}{f}} \right)^2$$





$$I = |u(r)|^2 = \frac{4a^2}{r^2} \left(\frac{\sin \frac{N\theta}{2}}{\sin \frac{\theta}{2}}\right)^2 \left(\frac{\sin \frac{kax}{f}}{\frac{kax}{f}}\right)^2$$

$$\frac{N\theta}{2} = \pi$$

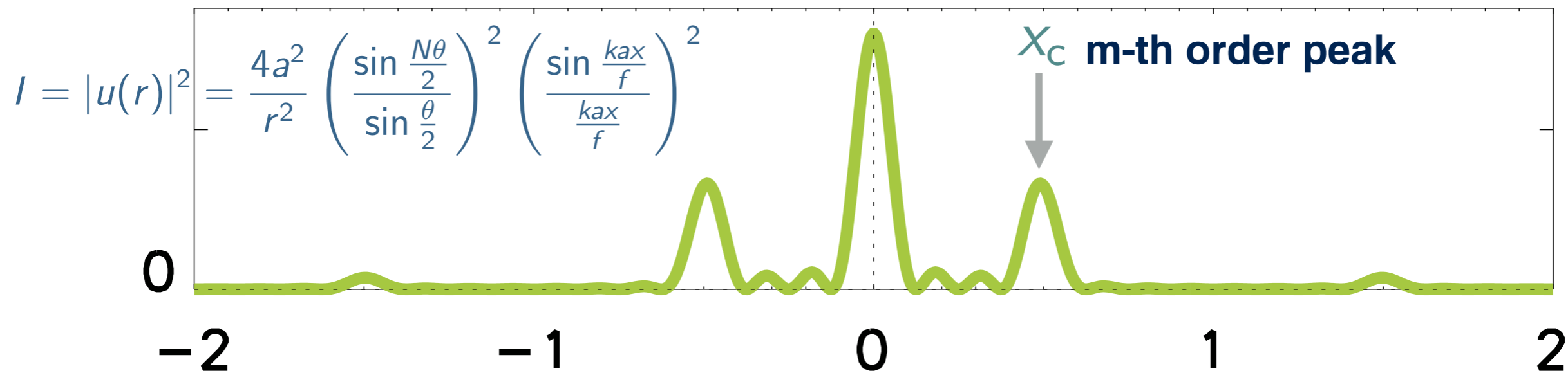
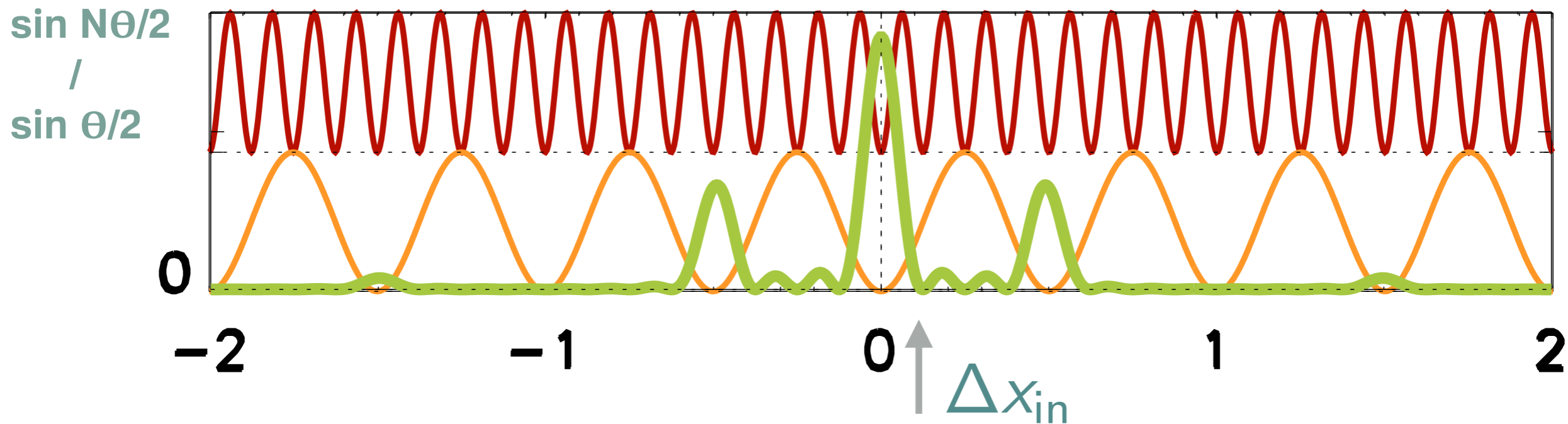
$$\theta = \frac{kxd}{f} \quad \frac{N kxd}{2 f} = \pi$$

first null

$$\Delta x_{in} = \frac{2f \pi}{N kd} = \frac{2f \lambda \pi}{N 2\pi d} = \frac{f \lambda}{N d}$$

line becomes sharper with N

$$I \sim N^2$$



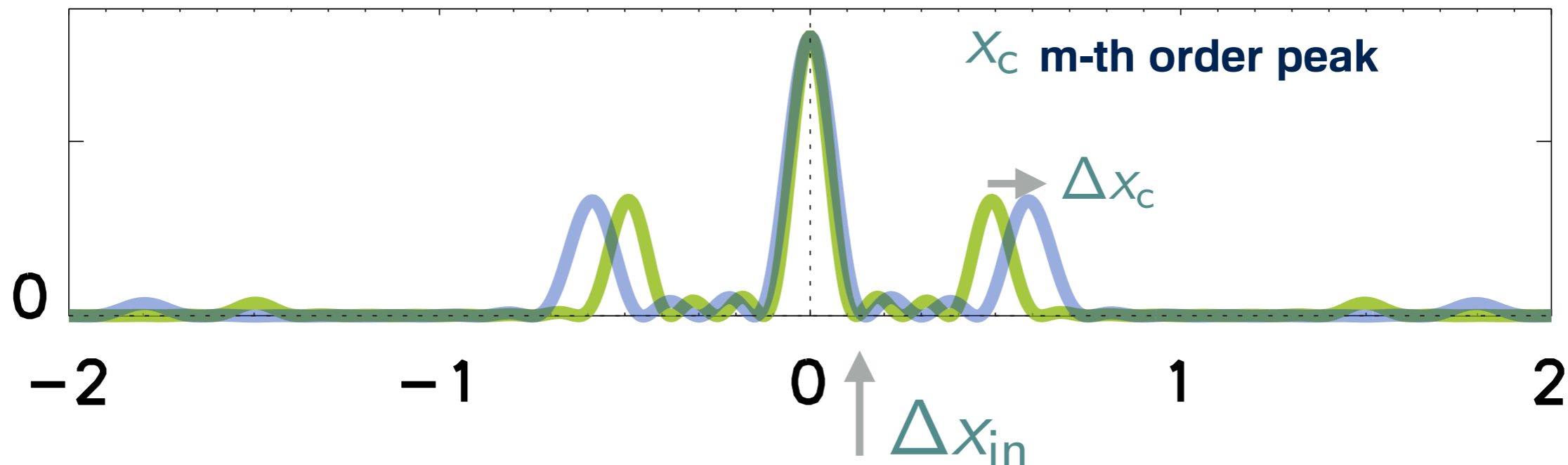
peak position is color dependent

$$\frac{\theta}{2} = m \cdot \pi$$

$$\theta = \frac{kxd}{f}$$

$$\frac{kx_c d}{2f} = m \cdot \pi$$

$$x_c = m \cdot \frac{2\pi f}{kd} = m \cdot \frac{2\pi \lambda f}{2\pi d} = m \cdot \frac{\lambda f}{d}$$



peak position is color dependent

in order to have a line resolved

$$x_c = m \cdot \frac{\lambda f}{d}$$

at different wavelength
peak is slightly off

$$\Delta x_c = m \cdot \frac{\Delta \lambda f}{d}$$

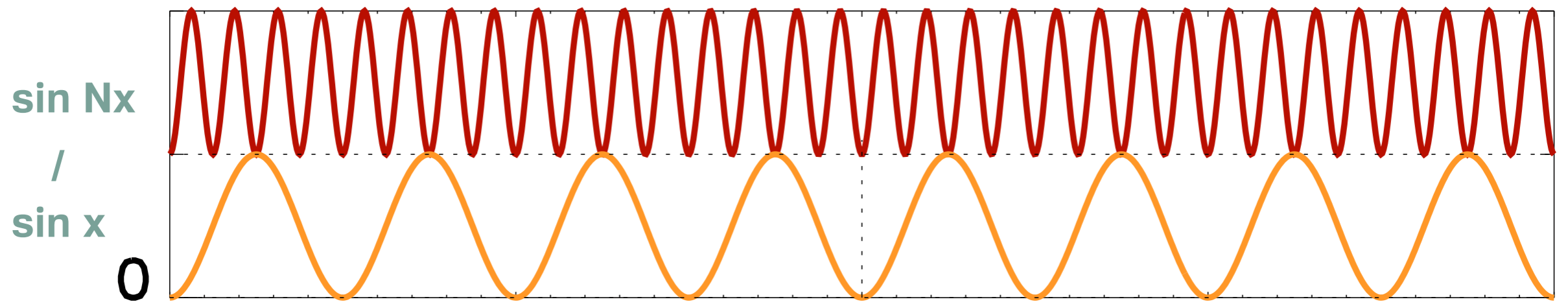
$$\Delta x_{in} < \Delta x_c$$

intrinsic

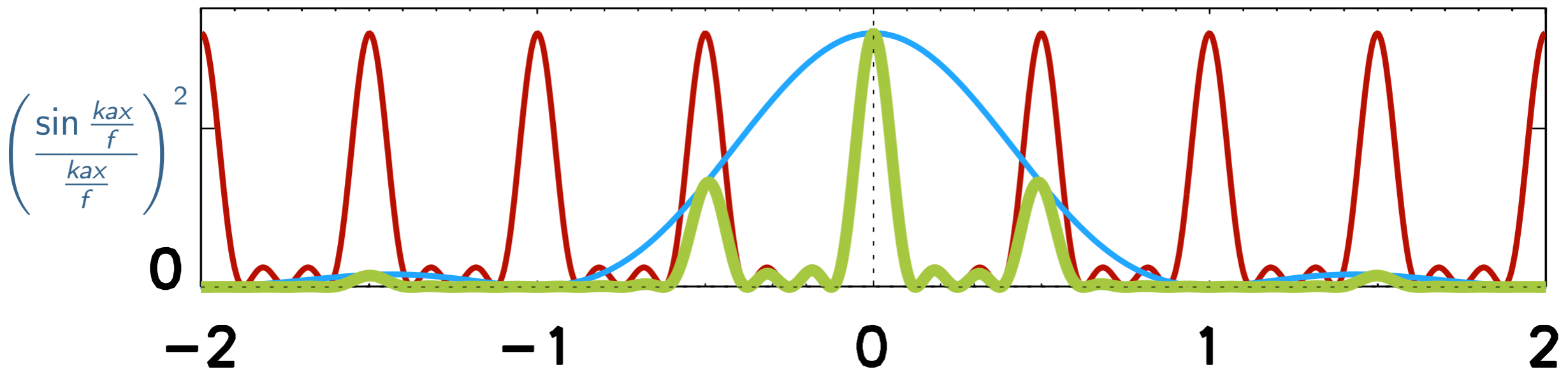
dispersion

$$\frac{f \lambda}{N d} < m \cdot \frac{\Delta \lambda f}{d}$$

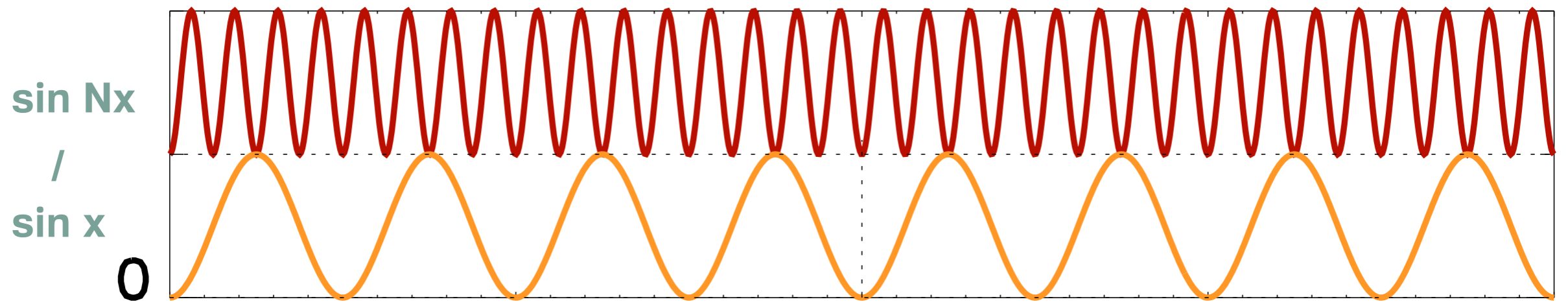
$$\frac{\lambda}{\Delta \lambda} < mN$$



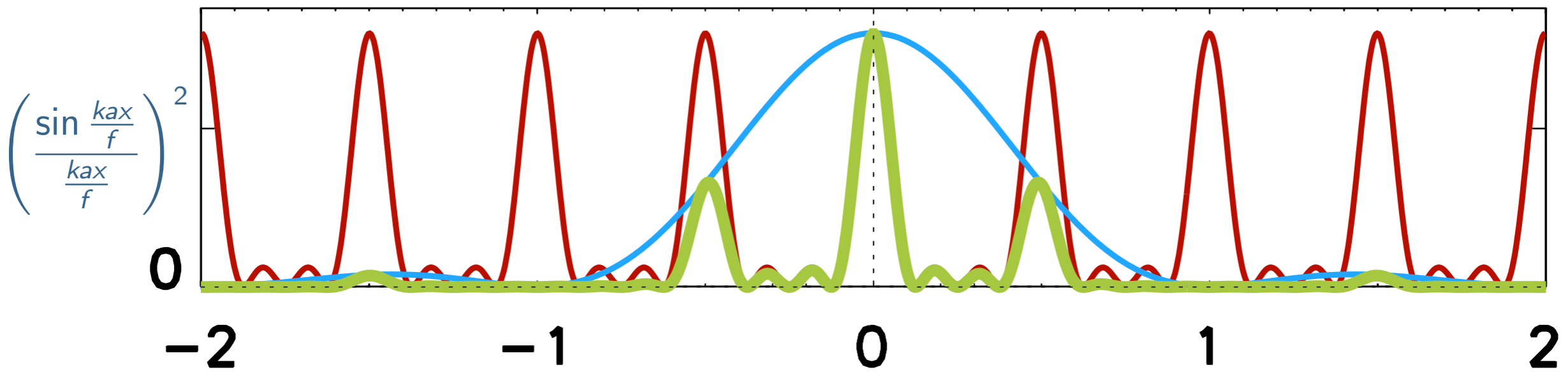
ka/f ←————→
 $kd/2f$ ←————→
 $Nkd/2f$ ←————→



$$I = \frac{4a^2 N^2}{r^2} \left(\frac{\sin \frac{Nkxd}{2f}}{N \sin \frac{kxd}{2f}} \right)^2 \left(\frac{\sin \frac{kax}{f}}{\frac{kax}{f}} \right)^2$$



ka/f ←→
 $kd/2f$ ←→
 $Nkd/2f$ ←→



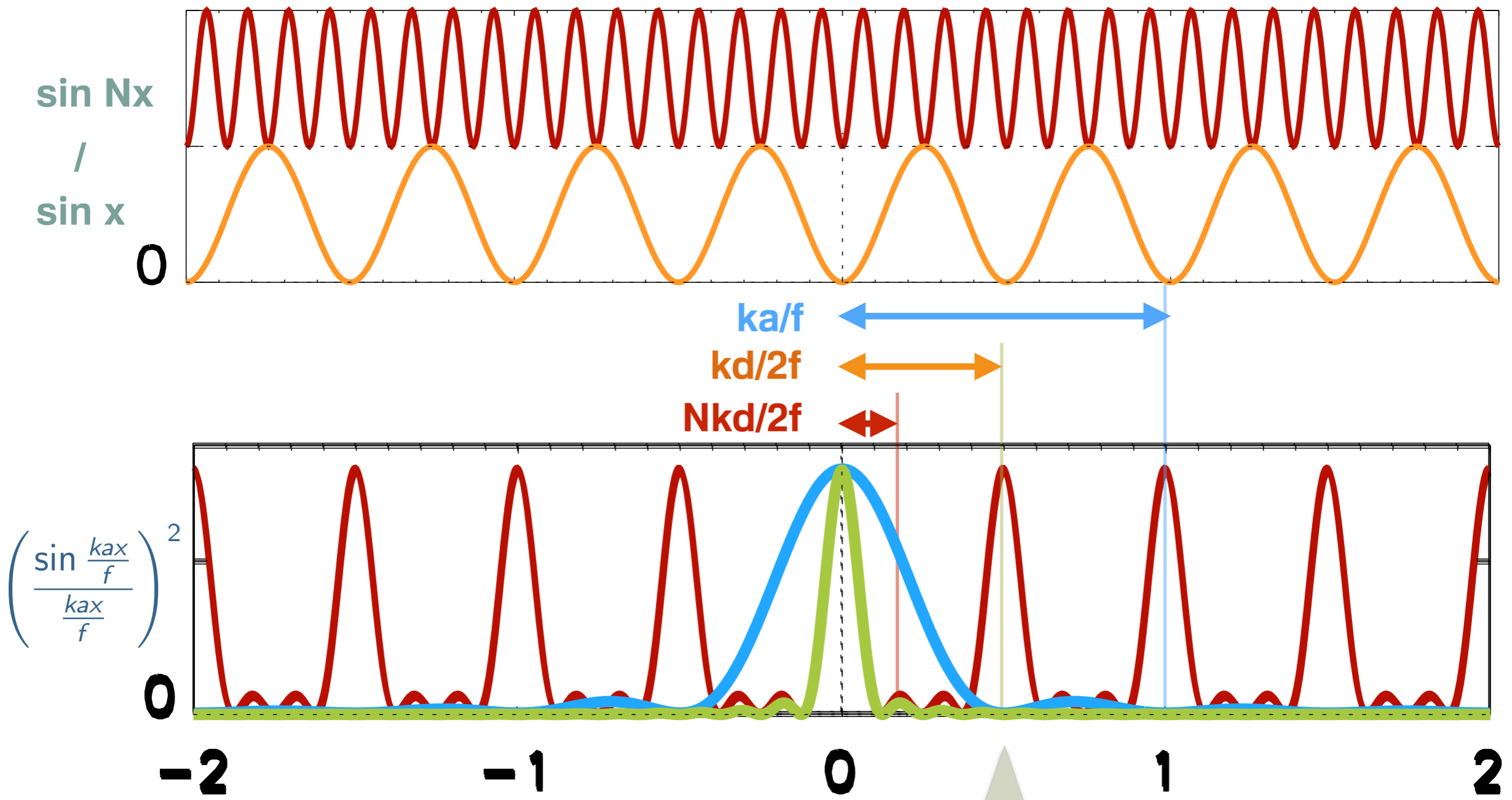
$\frac{kdx}{2f} = \ell\pi$

$\square = 1$

$\frac{kax}{f} = m\pi$

$\square = 0$

$$I = \frac{4a^2 N^2}{r^2} \left(\frac{\sin \frac{Nkxd}{2f}}{N \sin \frac{kxd}{2f}} \right)^2 \left(\frac{\sin \frac{kax}{f}}{\frac{kax}{f}} \right)^2$$



$$\frac{kdx}{2f} = \ell\pi$$

$$\square = 1$$

$$\frac{kax}{f} = m\pi$$

$$\square = 0$$

$d = 2a$ no side peak any more
 all missing order
 except $x = 0$ straight reflection
 what kind of grating?

Blazed grating

